# 6WCSCM Sixth World Conference on Structural Control and Monitoring

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**6WCSCM** 

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### Seismic Reduction of Monuments' Response Using Particle Dampers\*

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*Abstract*—This paper presents the results of an experimental study focusing on increasing the capacity of ancient multi-drum columns to resist lateral loading, without altering their overall appearance. The innovative approach proposed herein consists of replacing missing or heavily damaged drums by similar in-shape ones, with the difference that are internally hollow and they contain a number of steel spherical particles (particle damper). A column specimen was designed as a scaled replica of an existing ancient column made of marble and with a varying size of the empty space in the hollow drums. Different excitations, including actual earthquake recordings, were used to excite the specimen, with and without the proposed damper. It was found that a mass of particles equal to a small fraction of the mass of the column suffices to considerably reduce the vibrations induced.

Properly designed particle dampers can reduce significantly the response of ancient multi-drum columns to earthquake loads and increase their seismic efficiency with a minimal alteration of their appearance, compared to traditional restoration techniques.

#### I. INTRODUCTION

Multi-drum columns are parts of historical monuments that can be found around the Mediterranean and they are often exposed to earthquake loads. Anastylosis of monuments that are damaged includes substitution of missing or damaged parts with new material that resembles the original one. Unfortunately, replacing missing parts does not improve the capacity of the monuments to resist seismic actions, while most conventional methods available for increasing the monuments' capacity to resist seismic loads alter considerably their appearance. There is a need for new ways to protect and preserve the historic heritage without altering the overall appearance of the monuments.

Several analytical and experimental studies have examined the behavior of multi-drum columns under dynamic loads ([1]-[14]). Even though all these studies have provided useful information on the behavior of monuments they have not yielded much information about how to increase their seismic safety without altering their overall appearance.

A simple method that can increase the classical columns' seismic safety is the use of particle dampers. Particle dampers are simple passive devices that have been used to attenuate the vibration of structures. Their behavior has been studied since long ([15-32]). They consist of a container with particles that it is attached on the structure to be controlled. They start operating with the motion of the structure (primary system). The particles moving inside the container hit its walls exchanging momentum with the primary system and attenuating its oscillations.

This paper studies the effectiveness of particle dampers in increasing the seismic safety of monuments respecting their overall appearance. The damper takes the form of a classical drum looking exactly like the rest of the drums, but having a hollow part containing particles. A column-model replica of an ancient column of a Greek temple is subjected to different dynamic excitations including earthquake loads. Its response is measured with and without the damper considering the influence of the system's parameters.

#### II. EXPERIMENTAL SET-UP AND TESTING

A small marble model replica of an ancient column from the temple of Hephaestus in Athens was used (scale 1:8). The total weight and height of the marble column was 19.8 kg and 651 mm respectively. The column consisted of seven drums each with constant diameter (120 mm) and height (93 mm). The drums were simply placed one above the other without connection. The column was supported on a marble plate (140x140x20 mm) that was glued on a steel plate attached on a 3x5

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m shake. A safety structure was built around the marble column to contain the drums in case of overturning (Fig. 1). The motion of the column was recorded using accelerometers attached on the drums while a built in accelerometer recorded the motion of the table. Three dampers of different size were used with hollow part-diameter of 90, 80 and 65 mm, respectively. Steel spherical particles of 20 mm diameter were placed in the damper. The structure, both without and with damper, was excited by dynamic signals including actual earthquake records.



Figure 1: Experimental set-up.

#### III. RESPONSE OF MODEL COLUMN UNDER DYNAMIC LOADS

Initially a sinusoidal signal with frequencies in the range of 1 to 7 Hz was used to excite the column. The motion of the drums included rotation, sliding and rocking (Fig. 2). The main natural frequencies of the system were identified as 1.2, 1.6, 2.7 and 4.6 Hz, approximately (Fig. 3).

![](_page_5_Picture_5.jpeg)

Figure 2: Deformation of model column.

![](_page_6_Figure_0.jpeg)

Figure 3: Frequency response of absolute acceleration at top drum under sinusoidal excitation.

#### A. Response of column without damper under random excitation

Subsequently, the column was excited by a random signal of 10 sec duration, containing frequencies in the range of 1-10 Hz. After a few repetitions of the test it was realized that small imperfections were considerably influencing the response and no consistent pattern of the response could be identified. To increase the robustness of the results, the test was repeated several times and the average of the response was calculated. As a measure of the response of the structure, the root mean square (RMS) of the displacement of the structure with respect to the root mean square of the displacement of the base (RMS response ratio) was selected. The average RMS response ratio for the top drum in the direction of motion was 5.55 and the standard deviation of the mean 0.48. Fig. 4(a) presents the relative displacement of the top drum of the column where the motion was higher with respect to the base for a representative experiment with mid-response (RMS response ratio 4.7). The free vibration response of the column after the end of the excitation signal continued for a few seconds before coming to rest.

![](_page_6_Figure_4.jpeg)

Figure 4: Displacement of column's top drum (a) without damper; (b) with damper.

#### B. Response of column with damper under random excitation

The placement of the damper along height is an important parameter for its effectiveness. Since the motion of the column was higher at the upper part, the points of insertion of the damper were at the top of the column (replacing the 7<sup>th</sup> drum) and two drums below the top (replacing the 5<sup>th</sup> drum). Initially the damper with the large diameter hollow part (90 mm) replaced the 5th drum. Eight spherical particles were placed inside the damper corresponding to 1.33% of mass ratio m/M (mass of particles (m) with respect to the initial mass of the column (M)). The response of the structure was reduced more than 40% in comparison to that without the damper and was more predictable since small imperfections of the drum set-up did not affect the response considerably. The average RMS response ratio was 3.0 with standard deviation of the mean 0.1. Fig. 4(b) presents the relative displacement of the top drum in the direction of motion for a representative experiment with mid-response (RMS response ratio 2.8). At the end of the excitation, the motion of the column decreases faster than without the damper. Increasing the number of particles (Fig. 5) to sixteen (m/M = 2.66%) and to twenty two (m/M = 3.66%) or using the dampers with the smaller diameter hollow part reduced the effectiveness of the damper owing to the lack of momentum of the congested particles. Placing the damper at the top of the column replacing the 7<sup>th</sup> drum yielded also reduced response, except for the cases in which the damper slid more than usual producing less satisfactory results. However, when the damper replaced drums lower than the top one, the increased friction seemed to control the amount of sliding and, from that point of view, the response was more consistent.

![](_page_7_Picture_2.jpeg)

Figure 5: Damper with large diameter hollow part containing steel spherical particles.

#### C. Response of column under earthquake excitation

The model column was subjected to the Kalamata 1986 earthquake record, adjusted to the scale of the model. The frequency response of the acceleration of the top drum of the column without the particle damper is presented in Fig. 6(a) with the highest frequency response appearing below 2 Hz. The average RMS response ratio of the top column's drum without the damper was 5.82 (standard deviation of the mean 0.55). Fig. 7 presents the response displacement of the 7<sup>th</sup>, 5<sup>th</sup>, 3<sup>rd</sup> and 1<sup>st</sup> column's drum for a representative experiment with mid-response (RMS response ratio of the top drum = 4.78).

![](_page_7_Figure_6.jpeg)

Figure 6: Frequency response of absolute acceleration of column's top drum under Kalamata earthquake record: (a) without damper; (b) with damper.

Next, the damper with the large diameter hollow part containing eight steel spherical particles replaced the 5<sup>th</sup> drum. The column's top drum average response ratio was 2.48 with standard deviation of the mean 0.10. Fig. 8 presents the response displacement of the 7<sup>th</sup>, 5<sup>th</sup>, 3<sup>rd</sup> and 1<sup>st</sup> drum of a representative experiment with mid-response (RMS response ratio of the top drum = 2.22). The response in terms of displacement was reduced more than 50% in comparison to that without the damper. In addition, the motion of the column seized much earlier than without the damper. The frequency response of the acceleration of the top drum shows reduction of the response for frequencies below 4 Hz while there was an increase for some higher frequencies (Fig. 6(b)), which though have small affect in the motion of the structure.

![](_page_8_Figure_1.jpeg)

Figure 7: Displacement of column's drums without damper: (a) 7<sup>th</sup> drum; (b) 5<sup>th</sup> drum; (c) 3<sup>rd</sup> drum; (d) 1<sup>st</sup> drum.

![](_page_8_Figure_3.jpeg)

Figure 8: Displacement of column's drums with damper replacing the 5<sup>th</sup> drum: (a) 7<sup>th</sup> drum; (b) 5<sup>th</sup> drum; (c) 3<sup>rd</sup> drum; (d) 1<sup>st</sup> drum.

#### IV. CONCLUSIONS

This paper examined the effect of particle dampers on the response of classical columns under dynamic loads. The innovative approached used consisted of replacing an existing drum, that could have been damaged or missing, with a new one that resembled outside the original one but having a hollow inner part containing particles. It was found that when the damper is properly designed the response of the column can be reduced more than 40%. This new approach seems very promising owing to the increased seismic safety offered to monuments, without altering their overall appearance.

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